EUROPEAN PATENT SPECIFICATION

(54) **Equipment for and methods of locating the position of a fault on a power transmission line.**

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Description

This invention relates to equipment for and methods of locating the position of a fault on a power transmission line.

5 Satisfactory operation of known forms of such equipment, for example those using impedance to fault measuring techniques or adaptations thereof, relies on one or more of a number of assumptions which make them inaccurate in certain circumstances. The main assumptions made are as follows: that the transmission line conductors are ideally transposed; that the parameters of the network in which the transmission line is connected are known and constant; that the fault type can be determined; that shunt

10 capacitance of the line can be neglected; and that the phase of the current in the fault path can be determined.

It is an object of the present invention to provide an equipment for and method of locating the position of a fault on a power transmission line whose operation does not depend on any of the above assumptions.

According to a first aspect of the present invention there is provided an equipment for locating the

15 position of a fault on a power tranmission line between a first and a second end of said line comprising: first means for deriving first and second signals representative respectively of the voltage V_S and current I_S at said first end; second means for deriving third and fourth signals representative respectively of the voltage V_R and current I_R at said second end; and means for calculating the position of the fault utilising said first, second, third and fourth signals and equations of the form:

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$$X_f = A_S V_S - B_S I_S \; ; \text{ and}$$
$$X_f = A_R V_R - B_R I_R \; ,$$

where X_f is the fault voltage or current, A_S is a first transmission parameter of the line between the fault and

25 said first end, B_S is a second transmission parameter of the line between the fault and said first end, A_R is a first transmission parameter of the line between the fault and said second end, and B_R is a second transmission parameter of the line between the fault and said second end, each said transmission parameter being dependent upon the distance of the fault along the transmission line from a said end of the line.

30 In one particular equipment according to the invention where said power transmission line is a multi-phase power transmission line; said first and second means derive a set of said first, second, third and fourth signals in respect of each phase of said transmission line; and said means for calculating includes means for transforming said signals to produce corresponding sets of decoupled signals V_{Sn}, I_{Sn}, V_{Rn}, I_{Rn} and means for utilising each set of said decoupled signals in equations of the form:

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$$X_{fn} = A_{Sn} V_{Sn} - B_{Sn} I_{Sn} \; ; \text{ and}$$
$$X_{fn} = A_{Rn} V_{Rn} - B_{Rn} I_{Rn} \; ,$$

where $\underline{n}$ indicates the relevant said set.

40 According to a second aspect of the present invention there is provided a method of locating the position of a fault on a power transmission line between a first and a second end of said line comprising the steps of: deriving first and second signals representative respectively of the voltage V_S and current I_S at said first end; deriving third and fourth signals representative respectively of the voltage V_R and current I_R at said second end; and calculating the position of the fault utilising said first, second, third and fourth signals

45 and equations of the form:

$$X_f = A_S V_S - B_S I_S \; ; \text{ and}$$
$$X_f = A_R V_R - B_R I_R \; ,$$

50 where X_f is the fault voltage or current, A_S is a first transmission parameter of the line between the fault and said first end, B_S is a second transmission parameter of the line between the fault and said first end, A_R is a first transmission parameter of the line between the fault and said second end, and B_R is a second transmission parameter of the line between the fault and said second end, each said transmission parameter being dependent upon the distance of the fault along the transmission line from a said end of the

55 line.

In one particular method according to the invention where said power transmission line is a multi-phase power transmission line; the steps of deriving said first, second third and fourth signals comprise deriving a set of said first, second, third and fourth signals in respect of each phase of said transmisssion line; and the

step of calculating includes transforming said signals to produce corresponding sets of decoupled signals V_{Sn}, I_{Sn}, V_{Rn}, I_{Rn} and utilising each set of said decoupled signals in equations of the form:

$X_{fn} = A_{Sn}V_{Sn} - B_{Sn}I_{Sn}$; and

$X_{fn} = A_{Rn}V_{Rn} - B_{Rn}I_{Rn}$,

where n indicates the relevant set.

EP-A-0230801 discloses fault locating equipment which uses voltage and current data from both ends of the line. The equipment utilises two equations for the fault voltage, equations (1) and (2) at lines 37 and 38 on page 3 of EP-A-0230801. These equations are distinguished from the two equations specified in each of Claims 1 and 6 of the present application. In the equations of EP-A-0230801, transmission line parameters A_S and A_R of the equations of Claim 1 are set to unity. In other words the coefficient of each of deltaV$_A$ and deltaV$_B$ in the equations of EP-A-0230801 is unity, whereas in the equations of Claim 1 the coefficient of each of V_S and V_R is a transmission line parameter dependent upon the position of the fault. Thus, in essence, EP-A-0230801 makes the assumption that the transmission line is non-distributed, whereas the invention of the present application does not.

The invention will now be further explained and, one equipment for and method of locating the position of a fault on a power transmission line in accordance with the invention described by way of example, with reference to the accompanying drawings in which:

Figure 1 is a diagram illustrating a two port network;

Figure 2 is a schematic diagram of a power transmission line having a fault;

Figure 3 is a schematic diagram of the equipment; and

Figure 4 is a block schematic diagram showing the part of the equipment at one end of the transmission line in greater detail.

The invention makes use of the well known two port network equation. The two port network equation relates the voltage and current at one port of a two port network to the voltage and current at the other port, as follows:

$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A_1 B_1 \\ A_2 B_2 \end{bmatrix} \begin{bmatrix} V_2 \\ I_2 \end{bmatrix} \qquad (1),$$

where, as illustrated in Figure 1, V_1 and I_1 are the voltage and current respectively at one port of a two port network 1, V_2 and I_2 are the voltage and current respectively at the other port of the two port network 1, and A_1, A_2, B_1 and B_2 are the parameters, i.e. transfer functions, of the two port network 1. Multiplying out the matricies of equation (1) gives:

$V_1 = A_1V_2 + B_1I_2$ (2)

and $I_1 = A_2V_2 + B_2I_2$ (3).

The invention resides in the application of the two port network equation to the or each phase of a power transmission line having a fault in respect of the parts of the line on either side of the fault. Thus, referring to Figure 2, application of equation (2) to parts 3 and 5 of a power transmission line 7 on either side of a fault 9 produces an equation:

$V_f = A_SV_S - B_SI_S$ (4)

for part 3, and produces an equation:

$V_f = A_RV_R - B_RI_R$ (5)

for part 5; where: V_f is the fault voltage; V_S and I_S are the voltage and current respectively at the end 11 of the part 3 of the transmisson line 7 remote from the fault 9; V_R and I_R are the voltage and current respectively at the end 13 of the part 5 of the transmission line 7 remote from the fault 9; A_S and B_S are first and second transmission line parameters between the fault 9 and the end 11; and A_R and B_R are first and

second transmission line parameters between the fault 9 and the second end 13. From transmission line theory:

$A_S = \cosh(Tx)$
$B_S = Z_0 \sinh(Tx)$
$A_R = \cosh(T(L - x))$
$B_R = Z_0 \sinh(T(L - x))$ (6),

where T is the propagation constant of the line 7, $\underline{x}$ is the distance of the fault 9 along the transmission line 7 from the end 11, Z_0 is the characteristic impedance of the line 7 and $\underline{L}$ is the total length of the line 7 between the ends 11 and 13.

Equating the right-hand sides of equations (4) and (5) and substituting for A_S, B_S, A_R and B_R from equations (6) gives:

$$\cosh(Tx).V_S - Z_0 \sinh(Tx).I_S = \cosh(T(L-x)).V_R - Z_0 \sinh(T(L-x)).I_R$$

Expanding $\cosh(T(L-x))$ and $\sinh(T(L-x))$ gives:

$$\cosh(Tx).V_S - Z_0.\sinh(Tx).I_S = V_R(\cosh(TL).\cosh(Tx) - \sinh(TL).\sinh(Tx)) - I_R Z_0(\sinh(TL).\cosh(Tx) - \cosh(TL).\sinh(Tx)).$$

Rearranging gives:

$$-\cosh(Tx)(V_R.\cosh(TL) - I_R Z_0.\sinh(TL) - V_S) = \sinh(Tx).(I_R Z_0.\cosh(TL) - V_R.\sinh(TL) + I_S Z_0).$$

Therefore:

$$\tanh(Tx) = \frac{-(V_R.\cosh(TL) - I_R Z_0.\sinh(TL) - V_S)}{I_R Z_0.\cosh(TL) - V_R.\sinh(TL) + I_S Z_0}$$

Therefore:

$$x = \frac{\tanh^{-1}(-Q/P)}{T} \qquad (7),$$

where:

$$P = I_R Z_0.\cosh(TL) - V_R.\sinh(TL) + I_S Z_0 \qquad (8)$$

and:

$$Q = V_R.\cosh(TL) - I_R Z_0.\sinh(TL) - V_S \qquad (9).$$

Hence, if the values of V_S, I_S, V_R, I_R, Z_0, T and $\underline{L}$ are known, the distance $\underline{x}$ of the fault 9 along the transmission line 7 from the end 11 can be calculated from equations (7), (8) and (9). V_S, I_S, V_R and I_R can be measured at each end of the line and Z_0, T and $\underline{L}$ will be known for a given transmission line.

It is to be noted that equations (7), (8) and (9) hold irrespective of the type of the fault 9 and are indeterminate for a fault free healthy line. Furthermore, equations (7), (8) and (9) are independent of the fault path which may therefore be non-linear and still not affect the calculation of x. T and Z_0 cater for the non-transposition and shunt capacitance of the line and are not affected by the parameters of the network in which the transmission line is connected.

One example of an equipment for carrying out the method according to the invention will now be described with reference to Figure 3.

The equipment comprises, at each of the two ends 11 and 13 of the line 7, a voltage sensor 15A or 15B and current sensor 17A or 17B, for measuring the voltage V_S or V_R and current I_S or I_R at that end 11 or 13 of the line 7, an analogue to digital (A/D) converter 19A or 19B for converting the analogue signals output by the voltage and current sensors 15A, 17A or 15B, 17B into digital form, a microprocessor 21A or 21B which receives these digital signals and a display 23A or 23B. The line 7 is shown as interconnecting two power transmission systems R and S. The microprocessors 21A and 21B are interconnected so that each microprocesor 21A or 21B receives not only the digital voltage and current signals from the end at which it is situated, but also the digital voltage and current signals from the other end of the line 7. Each microprocessor 21A or 21B can therefore calculate $\underline{x}$ as defined by equations (7), (8) and (9) using the values of V_S, I_S, V_R and I_R input to it and the known values of Z_0, T and L. The, value of $\underline{x}$ is displayed on each of the displays 23.

Where the line 7 is a multiphase transmission line, the calculations are performed in respect of each phase of the transmitted power. However, in the case of a multiphase line the problem arises that the different phases will normally not be decoupled.

To overcome this problem a modal component transformation may be used, as described in an article by L.M.Wedephol entitled 'Application of matrix methods to the solution of travelling-wave phenomena in polyphase systems' published in December 1963 in Proc. IEE, Vol 110, No 12, at pages 2200 to 2212.

To this end the microprocessors 21A and 21B are arranged to multiply the voltage and current quantities V_S, I_S or V_R, I_R for each phase by an appropriate transformation matrix to produce corresponding sets of decoupled quantities V_{Sn}, I_{Sn} or V_{Rn}, I_{Rn} where $\underline{n}$ is 1, 2 etc. up to the number of phases in the system. These decoupled quantities are then utilised in respect of each phase of the line 7 in equations of the form:

$$V_{fn} = A_{Sn} V_{Sn} - B_{Sn} I_{Sn} \qquad (10)$$

and

$$V_{fn} = A_{Rn} V_{Rn} - B_{Rn} I_{Rn} \qquad (11),$$

where A_{Sn}, B_{Sn}, A_{Rn} and B_{Rn} are the model line parameters and

$$A_{Sn} = \cosh (T_n x)$$
$$B_{Sn} = Z_{On} \sinh (T_n X)$$
$$A_{Rn} = \cosh (T_n(L-x))$$
$$B_{Rn} = Z_{On} \sinh (T_n(L-x)) \qquad (12),$$

where T_n are the modal propagation constants of the line and Z_{On} are the characteristic modal impedances of the line. Equations (10), (11) and (12) are then worked in the same way as equations (4), (5) and (6) above to obtain the distance $\underline{x}$ of the fault along the line 7 from the end 11, as in equations (7), (8) and (9) above; that is:

$$x = \frac{\tanh^{-1} (-Q_n/P_n)}{T_n} \qquad (13),$$

where:

$$P_n = I_{Rn} Z_{On}.\cosh (T_n L) - V_{Rn}.\sinh (T_n L) + I_{Sn} Z_{On} \qquad (14)$$

and

$$Q_n = V_{Rn}.\cosh (T_n L) - I_{Rn}.Z_{On} \sinh (T_n L) - V_{Sn} \qquad (15).$$

One particular form of the equipment at each end of the line 7 will now be described in greater detail with reference to Figure 4. The equipment is for use with a three-phase transmission line. The three phase voltage and current signals V_a, V_b, V_c, I_a, I_b and I_c from line transformers (not shown) are fed, via an isolation transformer 33 and filters 35 for extracting the power frequency phase information, to a multiplexer 37. The output of the multiplexer 37 is then passed via a sample and hold gate 39 to an A/D converter 41. The resultant digitised signals are stored in a cyclic buffer in a random access memory 43 of a microprocessor 44 by a direct memory access unit 45. An input/output unit 46 is sampled continuously until a start signal indicating occurrence of fault is received from a line protection equipment, typically a distance relay, after which the process of sampling the phase voltage and current signals V_a, V_b, V_c, I_a, I_b, I_c continues until post fault data has been captured. The microprocessor 44 then carries out the necessary calculations. A keypad and alpha numeric display 47 are used to display and transfer the modal voltages and currents, to display the final distance to fault result calculated by the microprocessor and to enter the line parameters for storage in an electrically erasable programmable read only memory 49.

It will be understood that if the line 7 is a multi-circuit line there will be a set of modal components for each phase and each circuit. Thus for a single circuit three-phase line n will have values 1, 2 and 3 and for a double circuit three-phase line will have values 1 to 6.

It will be further understood that transformations other than a modal component transformation may be used for decoupling purposes in equipment and methods according to the invention. For example, the well known symmetrical component transformation might be used, for example, if the transmission line conductors were known to be ideally transposed.

It is also pointed out that whilst in the above explanation of the invention and in the equipment and method described by way of example, use of the voltage equation (2) is described, the current equation (3) could equally well be used.

Claims

1. An equipment for locating the position of a fault (9) on a power transmission line (7) between a first (11) and a second (13) end of said line (7) comprising: first means (15A,17A,19A) for deriving first and second signals representative respectively of the voltage V_S and current I_S at said first end (11); second means (15B,17B,19B) for deriving third and fourth signals representative respectively of the voltage V_R and current I_R at said second end (13); and means (21A,21B) for calculating the position of the fault (9) utilising said first, second, third and fourth signals and equations of the form:

$$X_f = A_S V_S - B_S I_S \; ; \text{ and}$$
$$X_f = A_R V_R - B_R I_R \, ,$$

where X_f is the fault voltage or current, A_S is a first transmission parameter of the line (7) between the fault (9) and said first end (11), B_S is a second transmission parameter of the line (7) between the fault (9) and said first end (11), A_R is a first transmission parameter of the line (7) between the fault (9) and said second end (13), and B_R is a second transmission parameter of the line (7) between the fault (9) and said second end (13), each said transmission parameter being dependent upon the distance of the fault (9) along the transmission line (7) from a said end (11 or 13) of the line (7).

2. An equipment according to Claim 1 wherein: X_f is the voltage at the fault (9); $A_S = \cosh(Tx)$; $B_S = Z_0 . \sinh(Tx)$; $A_R = \cosh(T(L-x))$ and $B_R = Z_0 . \sinh(T(L-x))$, where T is the propagation constant of said line (7), x is the distance of the fault (9) along the tranmission line (7) from said first end (11), Z_0 is the characteristic impedance of said line (7) and L is the total length of the line (7) between said first (11) and second (13) ends.

3. An equipment according to Claim 1 or Claim 2 wherein: said power transmission line (7) is a multi-phase power transmission line (7); said first (15A,17A,19A) and second (15B,17B,19B) means derive a set of said first, second, third and fourth signals in respect of each phase of said transmission line (7); and said means (21A,21B) for calculating includes means for transforming said signals to produce corresponding sets of decoupled signals V_{Sn}, I_{Sn}, V_{Rn}, I_{Rn} and means for utilising each set of said decoupled signals and equations of the form:

$$X_{fn} = A_{Sn} V_{Sn} - B_{Sn} I_{Sn} \; ; \text{ and}$$
$$X_{fn} = A_{Rn} V_{Rn} - B_{Rn} I_{Rn} \, ,$$

where n indicates the relevant said set.

4. An equipment according to Claim 3 wherein the transformation applied by said means for transforming is a modal component transformation.

5. An equipment according to any one of the preceding claims wherein said first (15A,17A,19A) and second (15B,17B,19B) means each include an analogue to digital converter (19A,19B) and said means for calculating (21A,21B) comprises a microprocessor (21A,21B).

6. A method of locating the position of a fault (9) on a power transmission line (7) between a first (11) and a second (13) end of said line (7) comprising the steps of: deriving first and second signals representative respectively of the voltage V_S and current I_S at said first end (11); deriving third and fourth signals representative respectively of the voltage V_R and current I_R at said second end (13); and calculating the position of the fault utilising said first, second, third and fourth signals and equations of the form:

$$X_f = A_S V_S - B_S I_S \; ; \text{ and}$$
$$X_f = A_R V_R - B_R I_R \, ,$$

where X_f is the fault voltage or current, A_S is a first transmission parameter of the line (7) between the fault (9) and said first end (11), B_S is a second transmission parameter of the line (7) between the fault (9) and said first end (11), A_R is a first transmission parameter of the line (7) between the fault (9) and said second end (13), and B_R is a second transmission parameter of the line (7) between the fault (9) and said second end (13), each said transmission parameter being dependent upon the distance of the fault (9) along the transmission line (7) from a said end (11 or 13) of the line (7).

7. A method according to Claim 6 wherein: X_f is the voltage at the fault (9); $A_S = \cosh (Tx)$; $B_S = Z_0.\sinh(Tx)$; $A_R = \cosh(T(L-x))$ and $B_R = Z_0.\sinh(T(L-x))$, where T is the propagation constant of said line (7), x is the distance of the fault (9) along the transmission line (7) from said first end (11), Z_0 is the characteristic impedance of said line (7) and L is the total length of the line (7) between said first (11) and second (13) ends.

8. A method according to Claim 6 or Claim 7 wherein: said power transmission line (7) is a multi-phase power transmission line (7); the steps of deriving said first, second, third and fourth signals comprise deriving a set of said first, second, third and fourth signals in respect of each phase of said transmisssion line (7); and the step of calculating includes transforming said signals to produce corresponding sets of decoupled signals V_{Sn}, I_{Sn}, V_{Rn}, I_{Rn} and utilising each set of said decoupled signals and equations of the form:

$$X_{fn} = A_{Sn} V_{Sn} - B_{Sn} I_{Sn} \; ; \text{ and}$$
$$X_{fn} = A_{Rn} V_{Rn} - B_{Rn} I_{Rn} \, ,$$

where, n indicates the relevant set.

9. A method according to Claim 8 wherein the transformation applied in the step of transforming is the modal component transformation.

10. A method according to any one of Claims 6 to 9 wherein said first, second, third and fourth signals are of digital form.

Patentansprüche

1. Anordnung zum Lokalisieren der Position eines Fehlers (9) auf einer Energieübertragungsleitung (7) zwischen einem ersten (11) und einem zweiten (13) Ende der Leitung (7), enthaltend: eine erste Einrichtung (15A, 17A, 19A) zum Ableiten erster und zweiter Signale jeweils zur Darstellung der Spannung V_S und des Stroms I_S am ersten Ende (11); eine zweite Einrichtung (15B, 17B, 19B) zum Ableiten dritter und vierter Signale jeweils zur Darstellung der Spannung V_R und des Stroms I_R am

zweiten Ende (13); und eine Einrichtung (21A, 21B) zum Berechnen der Position des Fehlern (9) unter Verwendung der ersten, zweiten, dritten und vierten Signale und von Gleichungen der Form:

$$X_f = A_S V_S - B_S I_S \text{ ; und}$$

$$X_f = A_R V_R - B_R I_R \text{ ,}$$

worin X_f die Fehlerspannung oder der Fehlerstrom ist, A_S ein erster Übertragungsparameter der Leitung (7) zwischen dem Fehler (9) und dem ersten Ende (11) ist, B_S ein zweiter Übertragungsparameter der Leitung (7) zwischen dem Fehler (9) und dem ersten Ende (11) ist, A_R ein erster Übertragungsparameter der Leitung (7) zwischen dem Fehler (9) und dem zweiten Ende (13) ist und B_R ein zweiter Übertragungsparameter der Leitung (7) zwischen dem Fehler (9) und dem zweiten Ende (13) ist, wobei jeder der Übertragungsparameter abhängig ist vom Abstand des Fehlers (9) längs der Übertragungsleitung (7) von dem jeweils genannten Ende (11 oder 13) der Leitung (7).

2. Anordnung nach Anspruch 1, bei der: X_f die Spannung beim Fehler (9) ist; $A_S = \cosh (Tx)$; $B_S = Z_0.\sinh (Tx)$; $A_R = \cosh (T(L-x))$ und $B_R = Z_0.\sinh (T(L-x))$, worin T die Fortpflanzungskonstante der Leitung (7) ist, x der Abstand des Fehlers (9) längs der Übertragungsleitung (7) vom ersten Ende (11) ist, Z_0 der Kennwiderstand der Leitung (7) ist und L die Gesamtlänge der Leitung (7) zwischen dem ersten (11) und dem zweiten (13) Ende ist.

3. Anordnung nach Anspruch 1 oder Anspruch 2, bei der: die EnergieÜbertragungsleitung (7) eine Mehrphasenenergie-Übertragungsleitung (7) ist; die erste (15A, 17A, 19A) und zweite (15B, 17B, 19B) Einrichtung einen Satz erster, zweiter, dritter und vierter Signale in bezug auf jede Phase der Übertragungsleitung (7) ableitet; und die Einrichtung (21A, 21B) zum Berechnen einer Einrichtung zum Umformen der Signale zum Gewinnen entsprechender Sätze entkoppelter Signale V_{Sn}, I_{Sn}, V_{Rn}, I_{Rn} und eine Einrichtung zum Verwenden jedes Satzes der entkoppelten Signale und von Gleichungen der Form enthält:

$$X_{fn} = A_{Sn} V_{Sn} - B_{Sn} I_{Sn} \text{ ; und}$$

$$X_{fn} = A_{Rn} V_{Rn} - B_{Rn} I_{Rn} \text{ ,}$$

worin n den jeweils relevanten Satz angibt.

4. Anordnung nach Anspruch 3, bei der die Transformation, die von der Einrichtung zum Umformen angewendet wird, eine Modalkomponententransformation ist.

5. Anordnung nach irgendeinem der vorangegangenen Ansprüche, bei der die erste (15A, 17A, 19A) und zweite (15B, 17B, 19B) Einrichtung jeweils einen Analog/Digital-Umsetzer (19A, 19B) enthält und die Einrichtung zum Berechnen (21A, 21B) einen Mikroprozessor (21A, 21B) enthält.

6. Verfahren zum Lokalisieren der Position eines Fehlers (9) auf eine Energieübertragungsleitung (7) zwischen einem ersten (11) und einem zweiten (13) Ende der Leitung (7), enthaltend die Schritte: Ableiten von ersten und zweiten Signalen jeweils darstellend die Spannung V_S und den Strom I_S bei dem ersten Ende (11); Ableiten von dritten und vierten Signalen jeweils darstellend die Spannung V_R und den Strom I_R an dem zweiten Ende (13); und Berechnen der Position des Fehlers unter Verwendung der ersten, zweiten, dritten und vierten Signale und von Gleichungen der Form:

$$X_f = A_S V_S - B_S I_S \text{ ; und}$$

$$X_f = A_R V_R - B_R I_R \text{ ,}$$

worin X_f die Fehlerspannung oder der Fehlerstrom ist, A_S ein erster Übertragungsparameter der Leitung (7) zwischen dem Fehler (9) und dem ersten Ende (11) ist, B_S ein zweiter Übertragungsparemeter der Leitung (7) zwischen dem Fehler (9) und dem ersten Ende (11) ist, A_R ein erster Übertragungsparameter der Leitung (7) zwischen dem Fehler (9) und dem zweiten Ende (13) ist und B_R ein zweiter Übertragungsparameter der Leitung (7) zwischen dem Fehler (9) und dem zweiten Ende (13) ist, wobei jeder der Übertragungsparameter abhängig ist vom Abstand des Fehlers (9) längs der Übertragungsleitung (7) von dem jeweiligen Ende (11 oder 13) der Leitung (7).

7. Verfahren nach Anspruch 6, bei dem: X_f die Spannung beim Fehler (9) ist; $A_S = \cosh$ (Tx); $B_S = Z_0 . \sinh$ (Tx); $A_R = \cosh$ (T(L-x)) und $B_R = Z_0 . \sinh$ (T(L-x)), worin T die Fortpflanzungskonstante der Leitung (7) ist, x der Abstand des Fehlers (9) längs der Übertragungsleitung (7) vom ersten Ende (11) aus ist, Z_0 der Kennwiderstand der Leitung (7) ist und L die Gesamtlänge der Leitung (7) zwischen dem ersten (11) und zweiten (13) Ende ist.

8. Verfahren nach Anspruch 6 oder Anspruch 7, bei dem: die Energieübertragungsleitung (7) eine Mehrphasenenergieübertragungsleitung (7) ist, die Schritte des Ableitens der ersten, zweiten, dritten und vierten Signale das Ableiten eines Satzes der ersten, zweiten, dritten und vierten Signale in bezug auf jede Phase der Übertragungsleitung (7) umfassen; und der Schritt des Berechnens die Umformung der Signale zum Gewinnen entsprechender Sätze entkoppelter Signale V_{Sn}, I_{Sn}, V_{Rn} und I_{Rn} umfaßt sowie die Verwendung jedes Satzes der entkoppelten Signale und von Gleichungen der Form umfaßt:

$$X_{fn} = A_{Sn}V_{Sn} - B_{Sn}I_{Sn} \; ; \; \text{und}$$
$$X_{fn} = A_{Rn}V_{Rn} - B_{Rn}I_{Rn} \, ,$$

worin n den relevanten Satz angibt.

9. Verfahren nach Anspruch 8, bei dem die Transformation, die beim Schritt des Umformens angewendet wird, die Modalkomponententransformation ist.

10. Verfahren nach irgendeinem der Ansprüche 6 bis 9, bei dem die ersten, zweiten, dritten und vierten Signale in digitaler Form vorliegen.

Revendications

1. Appareillage de localisation de la position d'un défaut (9) dans une ligne de transmission d'énergie (7) entre une première extrémité (11) et une seconde extrémité (13) de la ligne (7), comprenant un premier dispositif (15A, 17A, 19A) destiné à dériver des premiers et des seconds signaux représentatifs respectivement de la tension V_S et du courant I_S à la première extrémité (11), un second dispositif (15B, 17B, 19B) destiné à dériver des troisièmes et des quatrièmes signaux représentatifs respectivement de la tension V_R et du courant I_R à la seconde extrémité (13), et un dispositif (21A, 21B) destiné à calculer la position du défaut (9) par utilisation des premiers, seconds, troisièmes et quatrièmes signaux et d'équations de la forme

$$X_f = A_S V_S - B_S I_S,$$
$$X_f = A_R V_R - B_R I_R$$

X_f étant le courant ou la tension de défaut, A_S étant un premier paramètre de transmission de la ligne (7) entre le défaut (9) et la première extrémité (11), B_S étant un second paramètre de transmission de la ligne (7) entre le défaut (9) et la première extrémité (11), A_R étant un premier paramètre de transmission de la ligne (7) entre le défaut (9) et la seconde extrémité (13), et B_R étant un second paramètre de transmission de la ligne (7) entre le défaut (9) et la seconde extrémité (13), chaque paramètre de transmission dépendant de la distance du défaut (9), le long de la ligne de transmission (7), à ladite extrémité (11 ou 13) de la ligne (7).

2. Appareillage selon la revendication 1, dans lequel X_f est la tension au niveau du défaut (9), $A_S = ch(Tx)$, $B_S = Z_0.sh(Tx)$, $A_R = ch[T(L-x)]$, et $B_R = Z_0.sh[T(L-x)]$, T étant la constante de propagation de la ligne (7), x la distance du défaut (9) le long de la ligne de transmission (7) à la première extrémité (11), Z_0 étant l'impédance caractéristique de la ligne (7), et L étant la longueur totale de la ligne (7) entre la première extrémité (11) et la seconde extrémité (13).

3. Appareillage selon la revendication 1 ou 2, dans lequel la ligne de transmission d'énergie (7) est une ligne de transmission d'énergie polyphasée (7), le premier dispositif (15A, 17A, 19A) et le second dispositif (15B, 17B, 19B) dérivent d'un ensemble des premiers, seconds, troisièmes et quatrièmes signaux pour chaque phase de la ligne de transmission (7), et le dispositif (21A, 21B) de calcul comprend un dispositif destiné à transformer les signaux pour la formation d'ensembles correspondants de signaux découplés V_{Sn}, I_{Sn}, V_{Rn}, I_{Rn}, et un dispositif destiné à utiliser chaque ensemble de

signaux découplés et des équations de la forme

$$X_{fn} = A_{Sn}V_{Sn} - B_{Sn}I_{Sn}, \text{ et}$$
$$X_{fn} = A_{Rn}V_{Rn} - B_{Rn}I_{Rn}$$

n indiquant l'ensemble correspondant.

4. Appareillage selon la revendication 3, dans lequel la transformation appliquée par le dispositif de transformation est une transformation des composantes modales.

5. Appareillage selon l'une quelconque des revendications précédentes, dans lequel le premier dispositif (15A, 17A, 19A) et le second dispositif (15B, 17B, 19B) comprennent chacun un convertisseur analogique-numérique (19A, 19B) et le dispositif de calcul (21A, 21B) comprend un microprocesseur (21A, 21B).

6. Procédé de localisation de la position d'un défaut (9) dans une ligne de transmission d'énergie (7) entre une première extrémité (11) et une seconde extrémité (13) de la ligne (7), comprenant les étapes suivantes : la dérivation de premiers et de seconds signaux représentatifs respectivement de la tension V_S et du courant I_S à la première extrémité (11), la dérivation de troisièmes et quatrièmes signaux représentatifs respectivement de la tension V_R et du courant I_R à la seconde extrémité (13), et le calcul de la position du défaut à l'aide des premiers, seconds, troisièmes et quatrièmes signaux et d'équations de la forme

$$X_f = A_S V_S - B_S I_S,$$
$$X_f = A_R V_R - B_R I_R$$

X_f étant le courant ou la tension de défaut, A_S étant un premier paramètre de transmission de la ligne (7) entre le défaut (9) et la première extrémité (11), B_S étant un second paramètre de transmission de la ligne (7) entre le défaut (9) et la première extrémité (11), A_R étant un premier paramètre de transmission de la ligne (7) entre le défaut (9) et la seconde extrémité (13), et B_R étant un second paramètre de transmission de la ligne (7) entre le défaut (9) et la seconde extrémité (13), chaque paramètre de transmission dépendant de la distance du défaut (9), le long de la ligne de transmission (7), à ladite extrémité (11 ou 13) de la ligne (7).

7. Procédé selon la revendication 6, dans lequel X_f est la tension au niveau du défaut (9), $A_S = ch(Tx)$, $B_S = Z_0.sh(Tx)$, $A_R = ch[T(L-x)]$, et $B_R = Z_0.sh[T(L-x)]$, T étant la constante de propagation de la ligne (7), x la distance du défaut (9) le long de la ligne de transmission (7) à la première extrémité (11), Z_0 étant l'impédance caractéristique de la ligne (7), et L étant la longueur totale de la ligne (7) entre la première extrémité (11) et la seconde extrémité (13).

8. Procédé selon la revendication 6 ou 7, dans lequel la ligne de transmission d'énergie (7) est une ligne de transmission d'énergie polyphasée (7), les étapes de dérivation des premiers, seconds et quatrième signaux comprennent la dérivation d'un ensemble de premiers, seconds, troisièmes et quatrièmes signaux pour chaque phase de la ligne de transmission (7), et l'étape de calcul comprend la transformation des signaux pour la production d'ensembles correspondants de signaux découplés V_{Sn}, I_{Sn}, V_{Rn}, I_{Rn} et l'utilisation de chacun des ensembles de signaux découplés et d'équations de la forme

$$X_{fn} = A_{Sn}V_{Sn} - B_{Sn}I_{Sn}, \text{ et}$$
$$X_{fn} = A_{Rn}V_{Rn} - B_{Rn}I_{Rn}$$

n indiquant l'ensemble correspondant.

9. Procédé selon la revendication 10, dans lequel la transformation appliquée dans l'étape de transformation est une transformation de composantes modales.

10. Procédé selon l'une quelconque des revendications 6 à 9, dans lequel les premiers, seconds, troisièmes et quatrièmes signaux sont sous forme numérique.
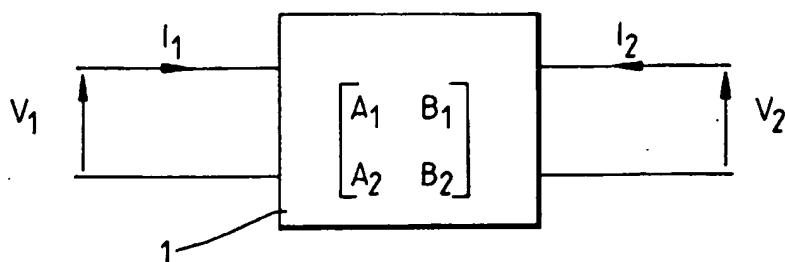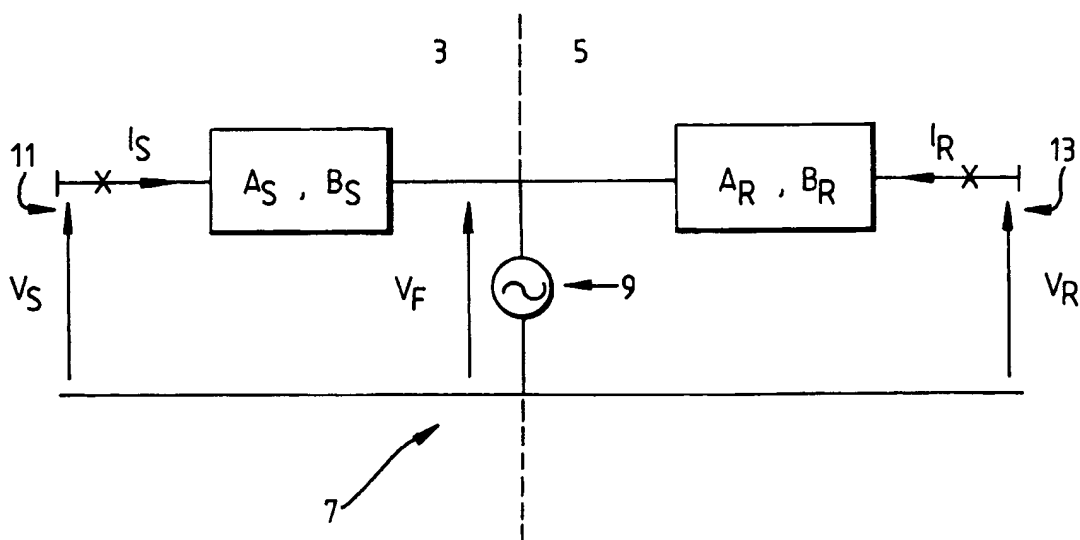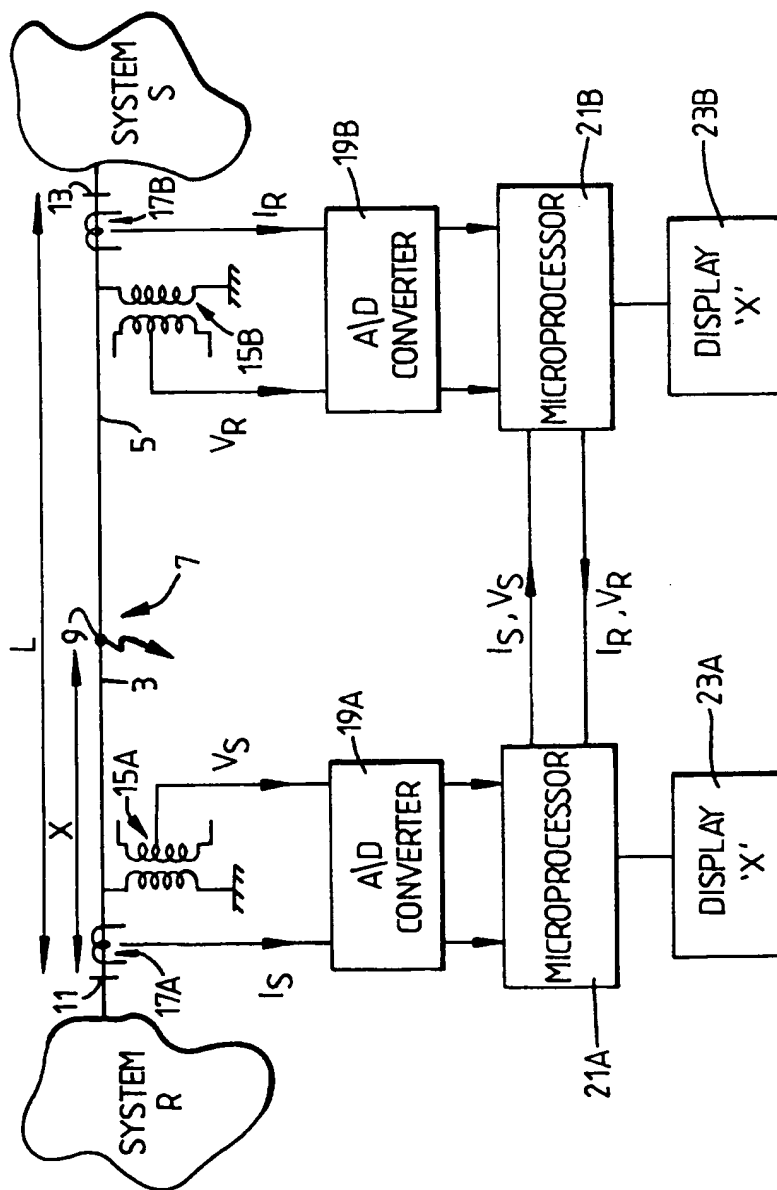
Fig.1.

Fig.2.

Fig.3.

Fig.4.